# Moment of Inertia of a Composite Area Steven Vukazich 

San Jose State University

## Recall the Parallel Axis Theorem



$$
I_{x}=\bar{I}_{x^{\prime}}+d^{2} A
$$

General Form

$$
I=\bar{I}+d^{2} A
$$

Centroidal Moment of Inertia

$$
\bar{I}_{x^{\prime}}=\iint y^{\prime 2} d A
$$

## Parallel Axis Theorem

If we know the moment of inertia of a body about an axis passing through its centroid, we can calculate the body's moment of inertia about any parallel axis

## If We Can Divide an Area into Simple Shapes With Known Centroid



Moment of Inertia of the entire area about the $x$ axis

$$
I_{x}=\sum I_{x i}=\sum \bar{I}_{x i}+\sum d_{y i}^{2} A_{i}
$$

## Tabulated Centroidal Moments of Inertia Can be Found in the Textbook

| Rexamb |  |  |
| :---: | :---: | :---: |
| Timasdo |  |  |
| Cinte |  |  |
| Smomicise |  |  |
| Qeneresiste |  |  |
| Ellupe |  |  |

## Tabulated Centroidal Moments of Inertia Can be Found in the Textbook

|  | Designation | $\begin{gathered} \text { Area } \\ \text { in }^{2} \end{gathered}$ | $\begin{aligned} & \text { Depth } \\ & \text { in. } \end{aligned}$ | $\begin{aligned} & \text { Width } \\ & \text { in. } \end{aligned}$ | Axis X-X |  |  | Axis $Y$ Y $Y$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | $\bar{I}_{\text {x }}$ in ${ }^{4}$ | $\bar{k}_{x}$, in. | $\bar{y}$, in. | $\bar{I}_{y}$, in ${ }^{4}$ | $\bar{k}_{\text {g }}$, in | $\bar{x}$, in. |
| W Shapes (Wide-Flange Shapes) | w $18 \times 76$ <br> W16 $\times 57$ <br> W $8 \times 31$ | $\begin{gathered} 22.3 \\ 16.8 \\ 11.2 \\ 9.12 \end{gathered}$ | $\begin{aligned} & 18.2 \\ & 16.4 \\ & 14.1 \\ & 8.00 \end{aligned}$ | $\begin{gathered} 11.0 \\ 7.12 \\ 6.77 \\ 8.00 \end{gathered}$ | $\begin{aligned} & 1330 \\ & 758 \\ & 355 \\ & 110 \end{aligned}$ | $\begin{aligned} & 7.73 \\ & 6.72 \\ & 5.87 \\ & 3.47 \end{aligned}$ |  | $\begin{aligned} & 152 \\ & 43.1 \\ & 26.7 \\ & 37.1 \end{aligned}$ | $\begin{aligned} & 2.61 \\ & 1.60 \\ & 1.55 \\ & 2.02 \end{aligned}$ |  |
| S Shapes <br> (American Standard <br> Shapes) | $\begin{aligned} & \mathrm{s} 18 \times 54.7 \dagger \\ & \mathrm{~S} 12 \times 31.8 \\ & \mathrm{~s} 10 \times 25.4 \\ & \mathrm{~S} 6 \times 12.5 \end{aligned}$ | $\begin{gathered} 16.0 \\ 9.31 \\ 7.45 \\ 3.66 \end{gathered}$ | $\begin{gathered} 18.0 \\ 12.0 \\ 10.0 \\ 6.00 \end{gathered}$ | $\begin{aligned} & 6.00 \\ & 5.00 \\ & 4.66 \\ & 3.33 \end{aligned}$ | $\begin{aligned} & 801 \\ & 217 \\ & 123 \\ & 22.0 \end{aligned}$ | $\begin{aligned} & 7.07 \\ & 4.83 \\ & 4.07 \\ & 2.45 \end{aligned}$ |  | $\begin{gathered} 20.7 \\ 9.33 \\ 6.73 \\ 1.80 \end{gathered}$ | $\begin{aligned} & 1.14 \\ & 1.14 \\ & 0.950 \\ & 0.702 \end{aligned}$ |  |
|  | $\begin{aligned} & \mathrm{C} 12 \times 20.7 \dagger \\ & \mathrm{Cl0} \mathrm{\times 15.3} \\ & \mathrm{CS} \times 11.5 \\ & \mathrm{C} 6 \times 8.2 \end{aligned}$ | $\begin{aligned} & 6.98 \\ & 4.48 \\ & 3.37 \\ & 2.39 \end{aligned}$ | $\begin{gathered} 12.0 \\ 10.0 \\ 8.00 \\ 6.00 \end{gathered}$ | $\begin{aligned} & 2.94 \\ & 2.20 \\ & 2.26 \\ & 1.92 \end{aligned}$ | $\begin{gathered} 129 \\ 67.3 \\ 32.5 \\ 13.1 \end{gathered}$ | $\begin{aligned} & 4.61 \\ & 3.87 \\ & 3.11 \\ & 2.34 \end{aligned}$ |  | $\begin{aligned} & 3.86 \\ & 2.27 \\ & 1.31 \\ & 0.687 \end{aligned}$ | $\begin{aligned} & 0.777 \\ & 0.711 \\ & 0.623 \\ & 0.536 \end{aligned}$ | $\begin{aligned} & 0.698 \\ & 0.634 \\ & 0.572 \\ & 0.512 \end{aligned}$ |
|  | $\mathrm{L} 6 \times 6 \times 1 \ddagger$ <br> $\mathrm{L} 4 \times 4 \times \frac{1}{2}$ <br> $\mathrm{L} 3 \times 3 \times \frac{1}{4}$ <br> $\mathrm{L} 6 \times 4 \times \frac{1}{2}$ <br> L5 $\times 3 \times \frac{1}{2}$ <br> $\mathrm{L} 3 \times 2 \times \frac{1}{4}$ | $\begin{gathered} 11.0 \\ 3.75 \\ 1.44 \\ 4.75 \\ 3.75 \\ 1.19 \end{gathered}$ |  |  | $\begin{gathered} 35.4 \\ 5.52 \\ 1.23 \\ 17.3 \\ 9.43 \\ 1.09 \end{gathered}$ | $\begin{aligned} & 1.79 \\ & 1.21 \\ & 0.926 \\ & 1.91 \\ & 1.58 \\ & 0.953 \end{aligned}$ | $\begin{aligned} & 1.86 \\ & 1.18 \\ & 0.836 \\ & 1.98 \\ & 1.74 \\ & 0.980 \end{aligned}$ | 35.4 <br> 5.52 <br> 1.23 <br> 6.22 <br> 2.55 <br> 0.390 | $\begin{aligned} & 1.79 \\ & 1.21 \\ & 0.926 \\ & 1.14 \\ & 0.824 \\ & 0.569 \end{aligned}$ | $\begin{aligned} & 1.86 \\ & 1.18 \\ & 0.836 \\ & 0.981 \\ & 0.746 \\ & 0.457 \end{aligned}$ |

## Example Problem



## Divide Area into Simple Composite Shapes



## Find the Area, Location of Centroid, and the Centroidal Moment of Inertia of Each Shape



## Find the Area, Location of Centroid, and the Centroidal Moment of Inertia of Each Shape



## Find Area and Location of Centroid of Each Shape Relative to Reference Coordinate Axes



## Find Area and Location of Centroid of Each Shape Relative to Reference Coordinate Axes



## Find Area and Location of Centroid of Each Shape Relative to Reference Coordinate Axes



## Use Parallel Axis Theorem to Complete Table for Semicircle



$$
I_{x}=\bar{I}_{x^{\prime}}+d_{y}^{2} A
$$

$$
\bar{I}_{x^{\prime}}=I_{x}-d_{y}^{2} A
$$

$$
\bar{I}_{x \prime}=\left(\frac{\pi}{8}-\frac{8}{9 \pi}\right) r^{4}
$$

$\bar{I}_{x \prime}=\frac{1}{8} \pi r^{4}-\left(\frac{4 r}{3 \pi}\right)^{2}\left(\frac{\pi r^{2}}{2}\right)$

## Find Area and Location of Centroid of Each Shape Relative to Reference Coordinate Axes



$$
\bar{I}_{y_{3},}=-\left(\frac{\pi}{8}-\frac{8}{9 \pi}\right) r^{4}=-\left(\frac{\pi}{8}-\frac{8}{9 \pi}\right)\left(2^{4}\right)=-1.75610 \text { in }^{4}
$$

## Find the Moment of Inertia about the $x$ axis

$$
\begin{aligned}
& \bar{I}_{x_{1},}=5.25 \text { in }^{4} \\
& d_{y 1}=-2.0 \text { in } \\
& A_{1}=10.5 \mathrm{in}^{2} \\
& \bar{I}_{x 2 \prime}=21.333 \mathrm{in}^{4} \\
& \bar{I}_{x 3^{\prime}}=-6.28318 \text { in }^{4} \\
& d_{y 2}=-5.0 \text { in } \\
& d_{y 3}=-3 \text { in } \\
& A_{2}=16 \text { in }^{2} \\
& A_{3}=-6.2832 \text { in }^{2} \\
& I_{x}=\sum \bar{I}_{x i}+\sum d_{y i}^{2} A_{i} \\
& I_{x}=20.30+385.4514=405.75 \text { in }^{4}
\end{aligned}
$$

## Find the Moment of Inertia about the $\boldsymbol{y}$ axis

$$
\begin{aligned}
& \begin{array}{|c|l|l|}
\bar{I}_{y 1^{\prime}}=28.5833 \mathrm{in}^{4} & \bar{I}_{y 2^{\prime}}=21.333 \mathrm{in}^{4} \quad \bar{I}_{y 3 \prime}=-1.75610 \mathrm{in}^{4} \\
\hline
\end{array} \\
& d_{x 1}=4.67 \mathrm{in} \\
& d_{x 2}=5.0 \text { in } \\
& d_{x 3}=5.1512 \text { in } \\
& A_{1}=10.5 \mathrm{in}^{2} \\
& A_{2}=16 \text { in }^{2} \\
& A_{3}=-6.2832 \text { in }^{2} \\
& I_{y}=\sum \bar{I}_{y i}+\sum d_{x i}^{2} A_{i}
\end{aligned}
$$

| Shape | $\bar{I}_{y i \prime}$ | $d_{x i}$ | $A_{i}$ | $d_{x i}^{2} A_{i}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 28.5833 | 4.67 | 10.5 | 919.0274 |
| 2 | 21.3333 | 5.0 | 16.0 | 400.0 |
| 3 | -1.75610 | 5.1512 | -6.28318 | -166.7233 |
| $\sum$ | 48.1606 |  |  | 1152.3041 |

$$
I_{y}=48.1606+1152.3041=1200.46 \mathrm{in}^{4}
$$

